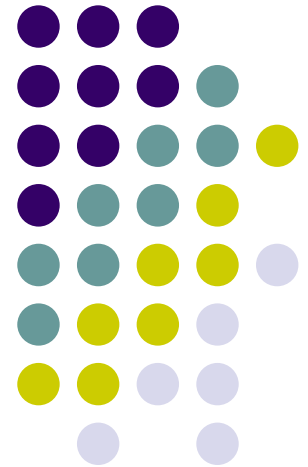
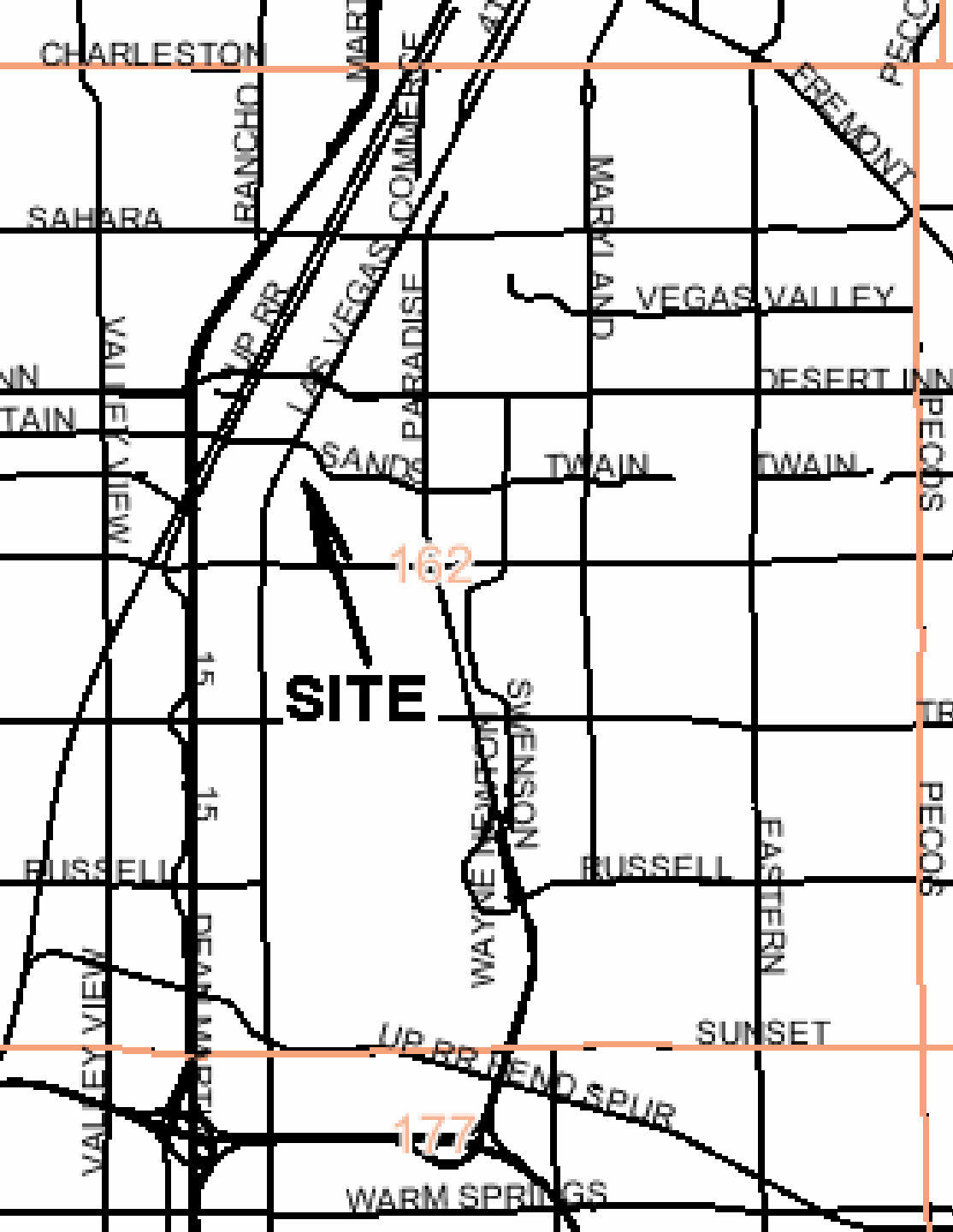


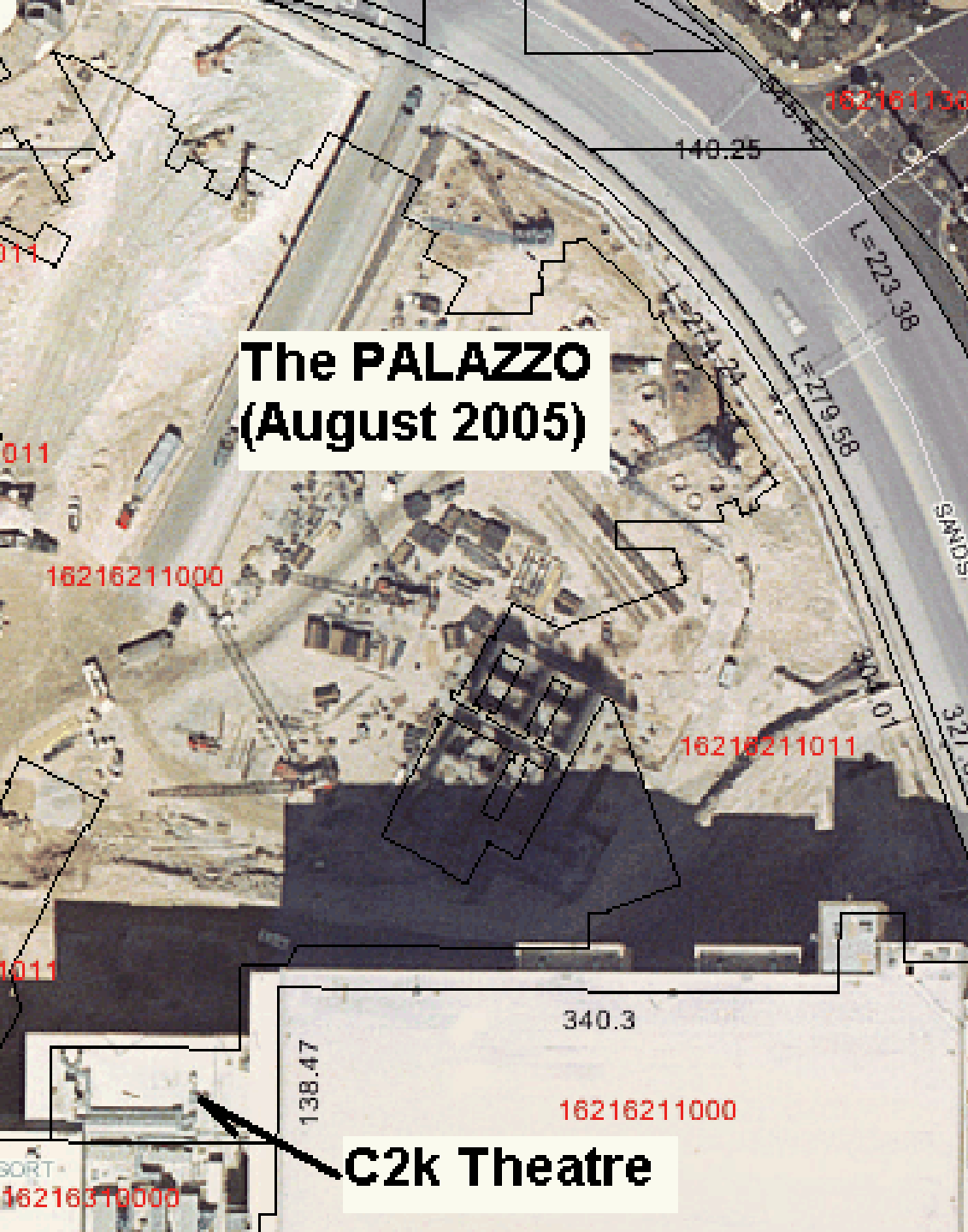
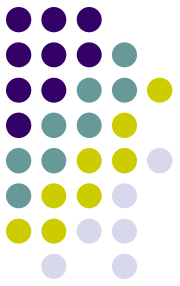
Observations From The Instrumentation of a Micropiled and Tied Back Reticulated Grid

Walter E. Vanderpool, P.E.
Senior Geotechnical Engineer
Terracon Consultants, Inc.





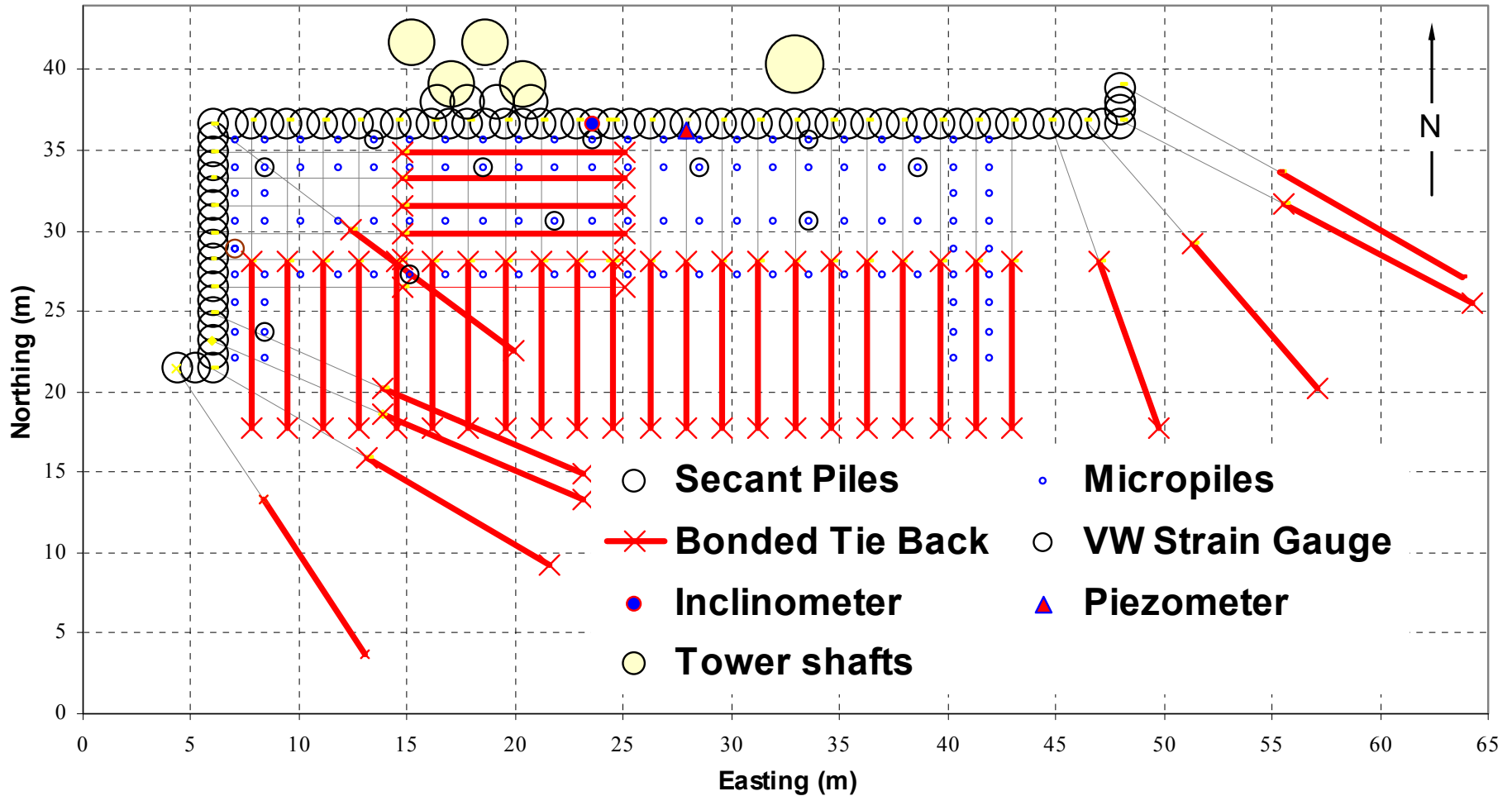
- Site: The C2K Theatre at the Palazzo
- 370 kN wall load at the crest of a 15.3 m excavation
- Theatre construction concurrent with excavation and tower construction



**The PALAZZO
(August 2005)**

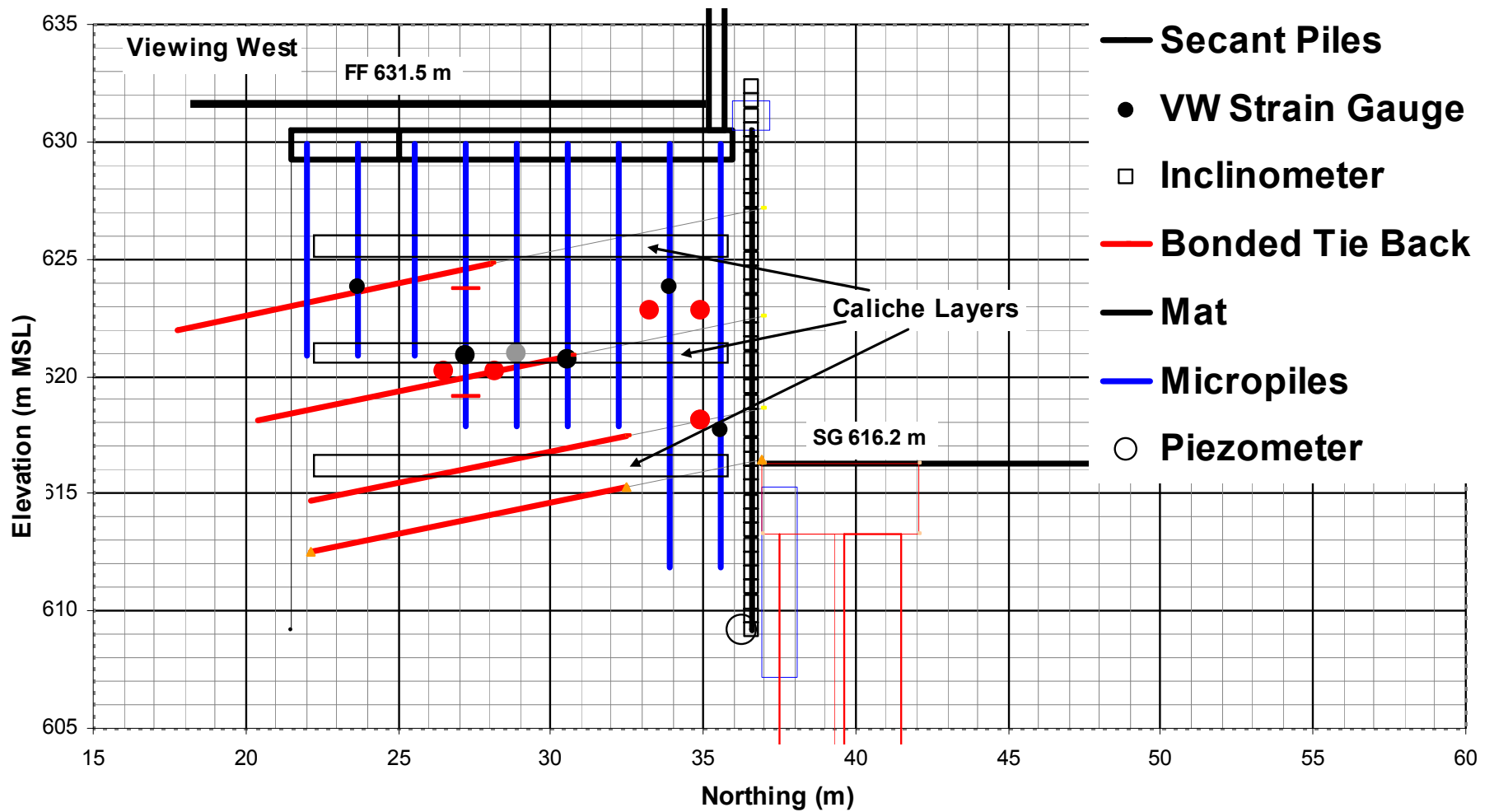
C2k Theatre

- Site excavation began 9/1/04
- Theatre construction began 11/25/04
- Secant pile installation began 12/6/04
- Underpinning installed 12/11/04
- Secant piling complete 12/16/04
- Theatre structure frame complete 3/14/05



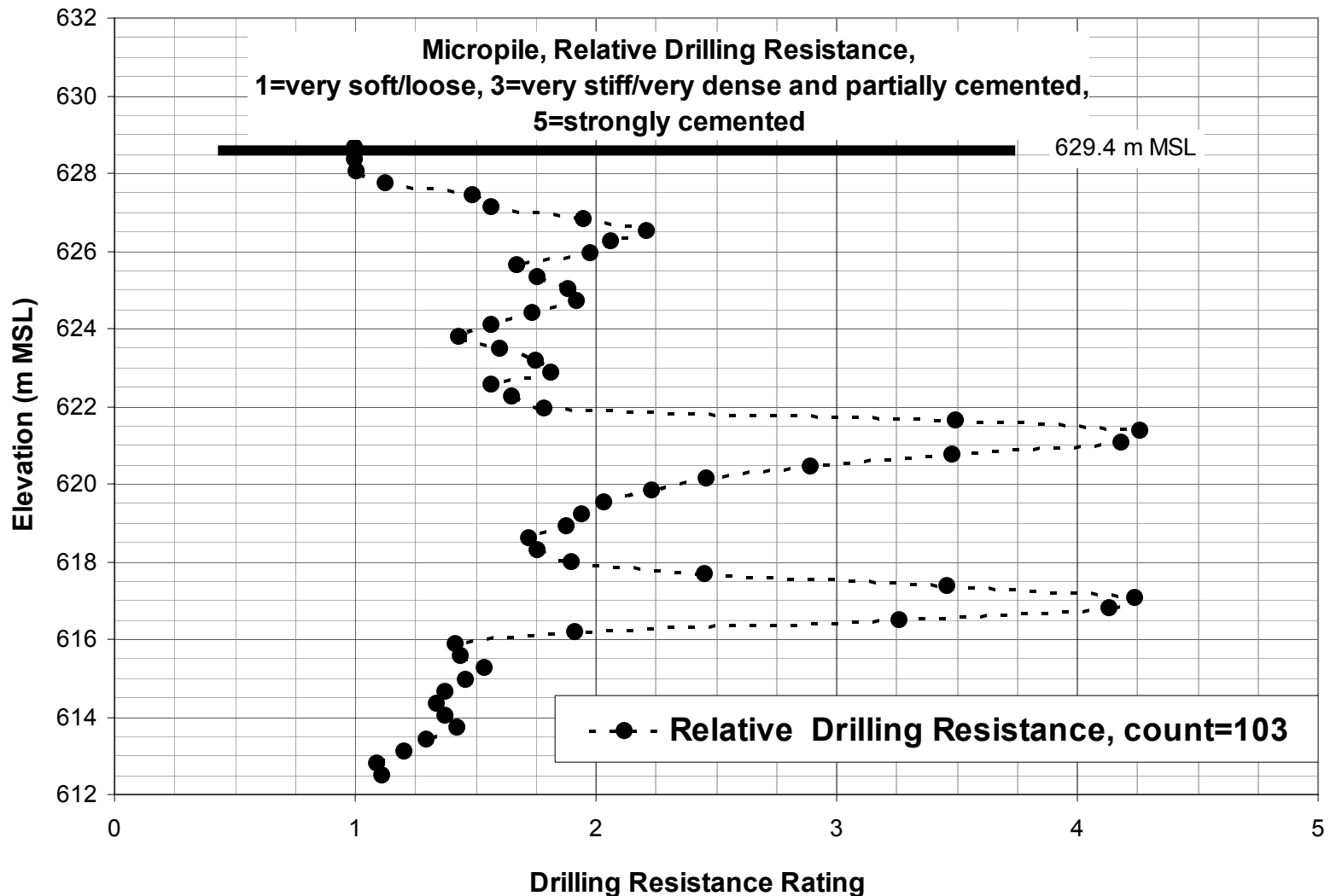
- Reticulated group plan
- VW gauge locations
- Micropile locations

- Tieback locations
- Foundation shafts for cantilevered tower

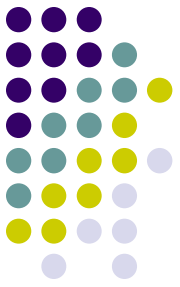


- Reticulated group profile
- VW gauge locations
- Micropile locations
- Tieback locations

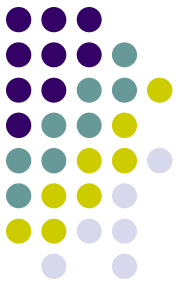
- Reticulated tieback intersections
- Cemented beds
- Piezometer location



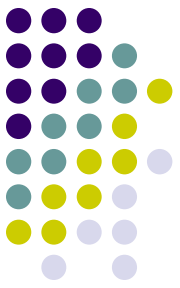
- Relative top-drive hammer drilling resistance
- Measured by rate of advance
- Subjectively interpreted relative to geotechnical logging



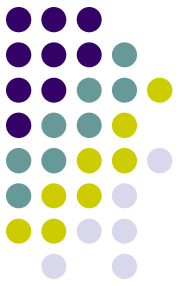
- Flush grout injection drilling
- VW strain gauge
- Insertion by fiberglass rod



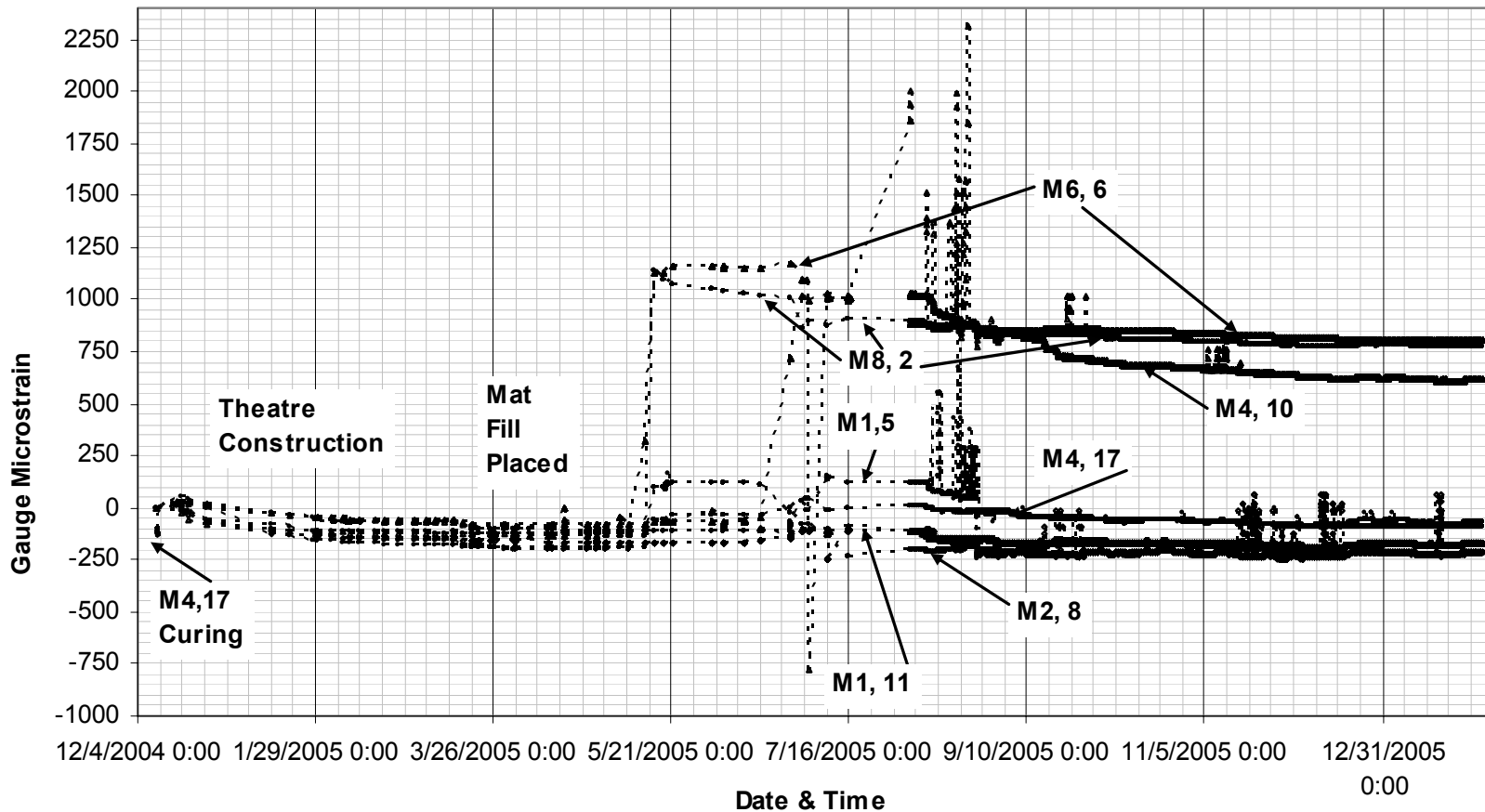
- Inclinator at P1-015NS
- Piezometer at P1-013S
- Cemented layer at approximately elevation 626.5 m to 625 m MSL



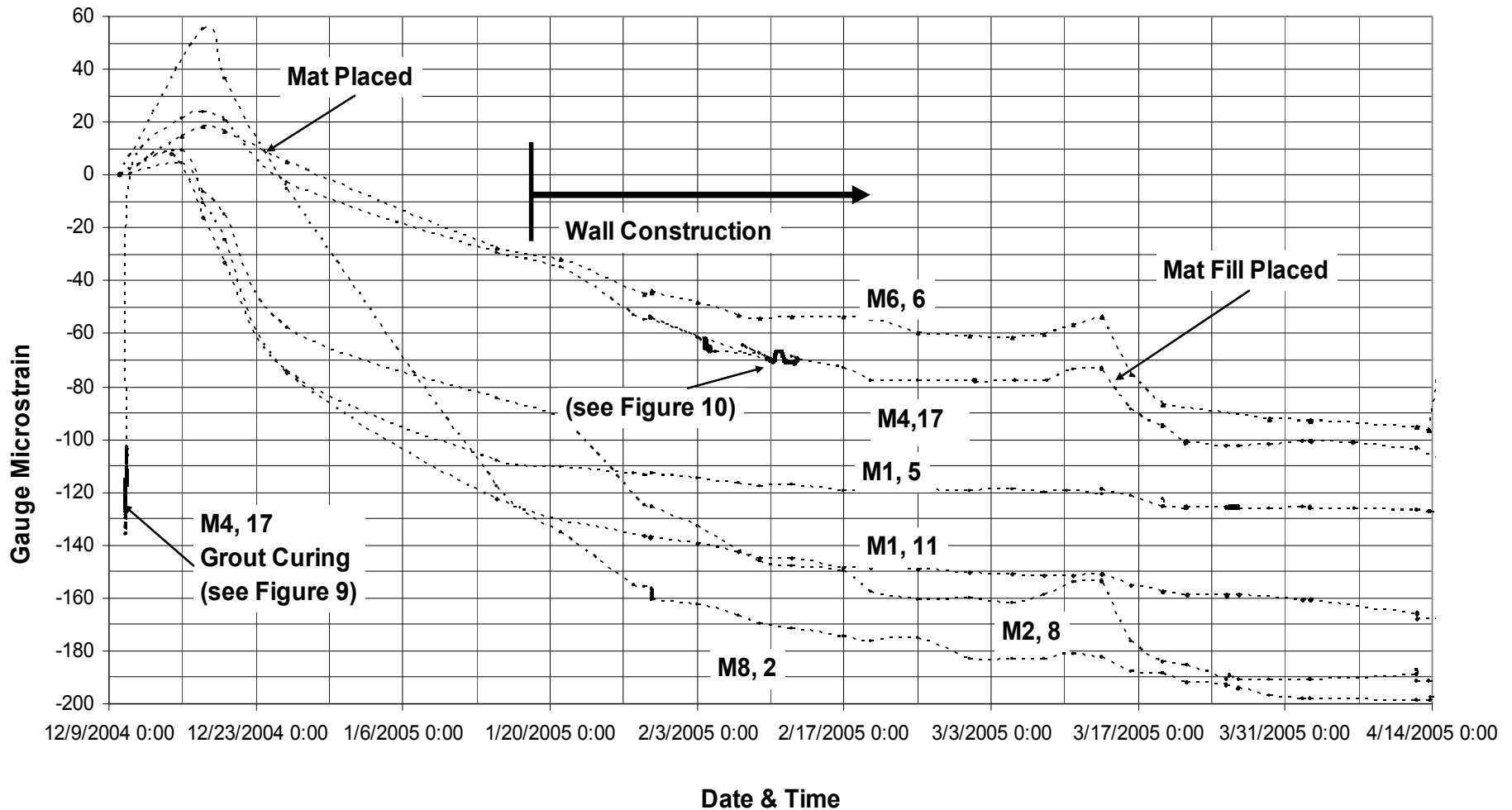
- Notch at tower cantilever
- Theatre wall
36.3 m - wide by
32 m - high by
457mm - thick
- Carbonate precipitate at tie-backs



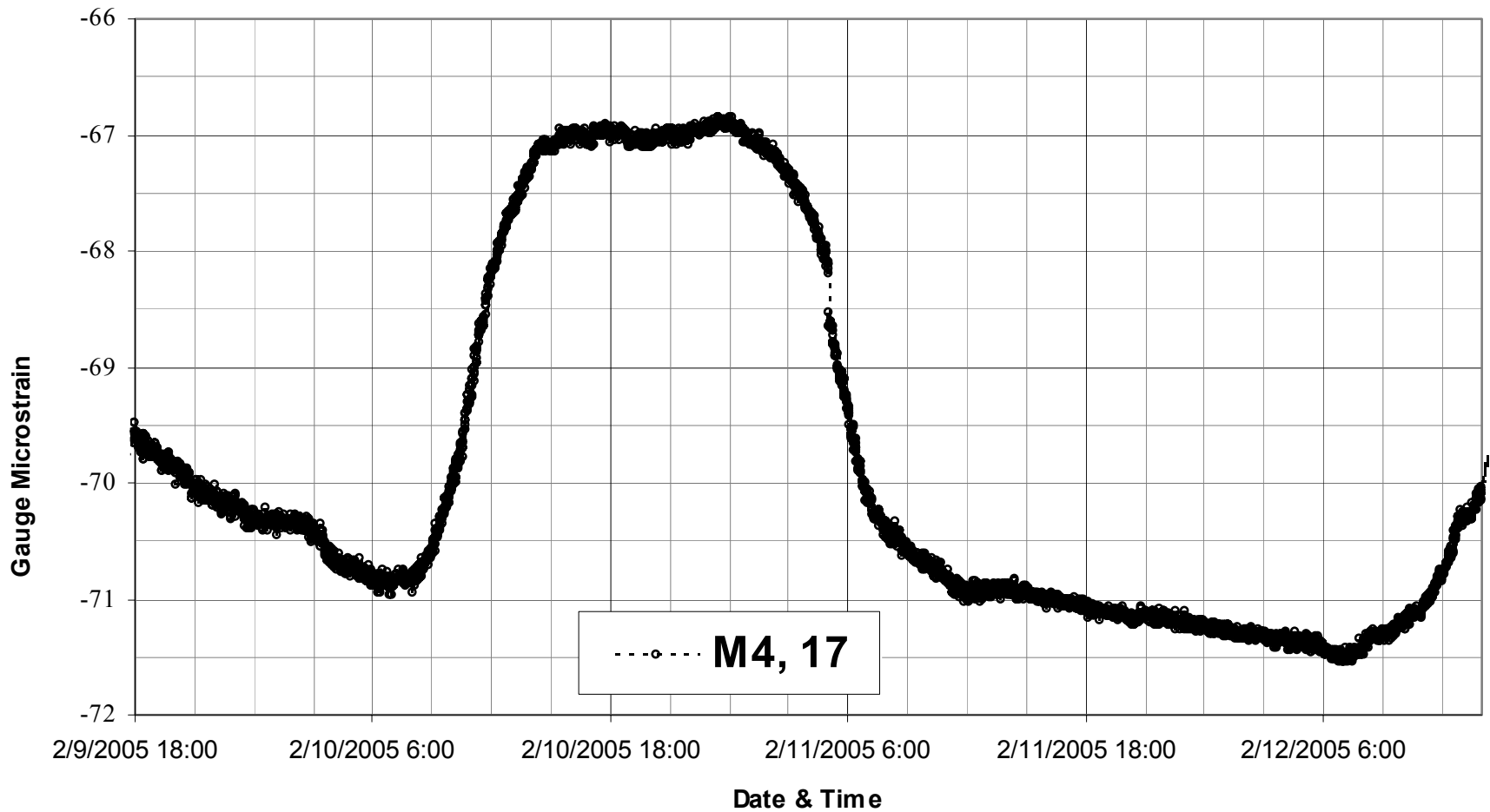
- Tower shaft group at cantilever



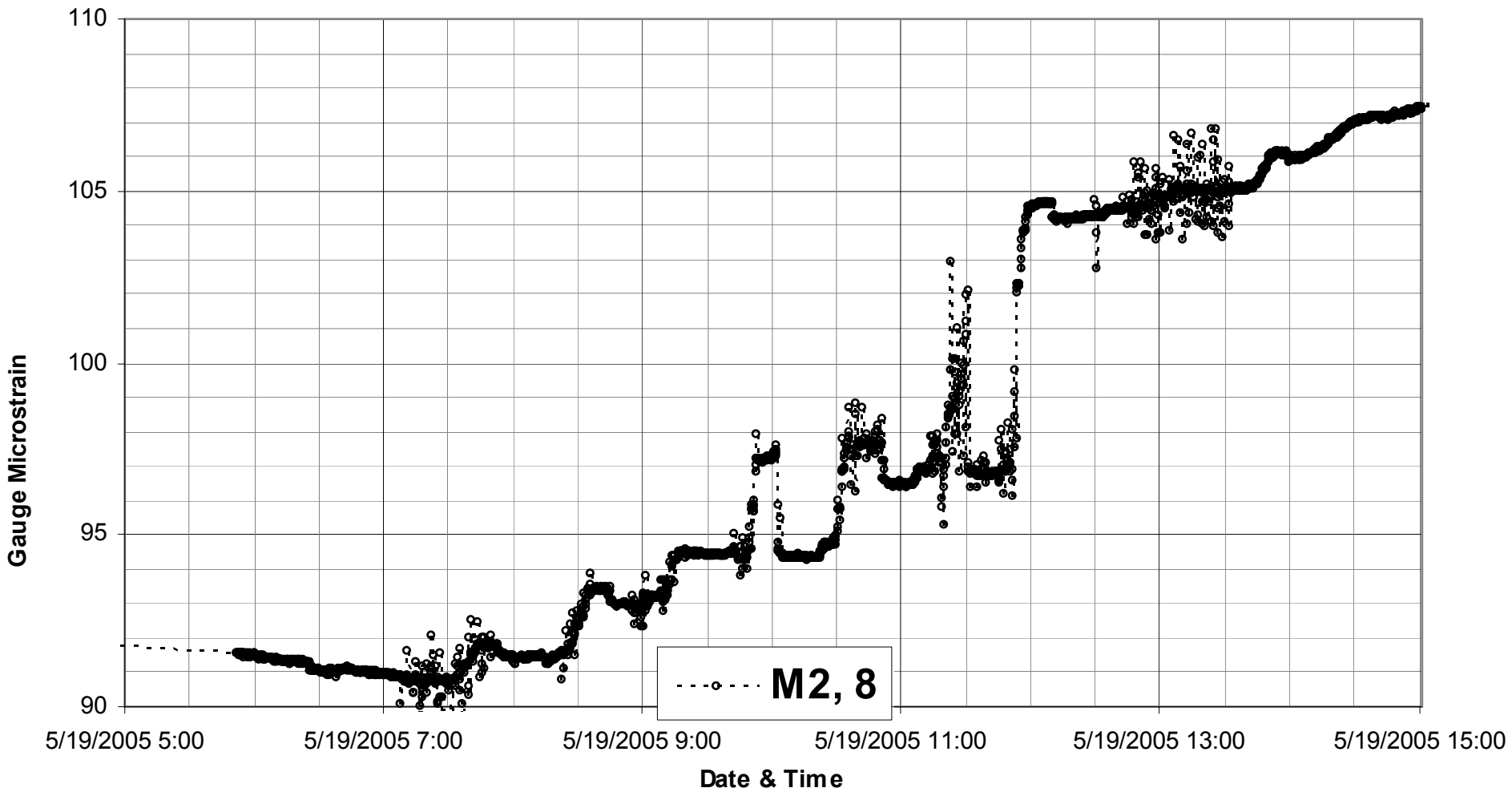
- Micropile strain history
- VW strain gauge data record
- Installation 12/04 through completion 1/06



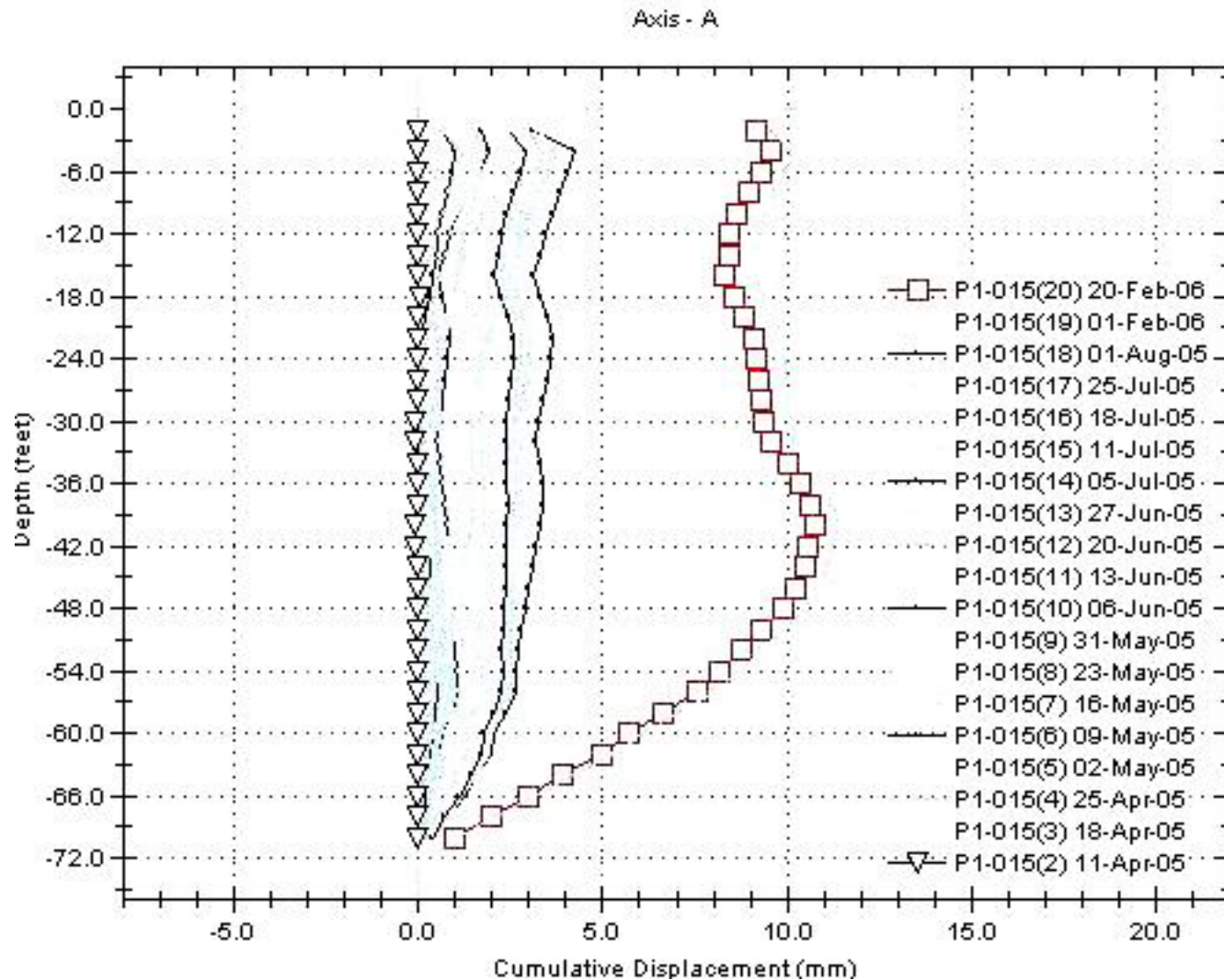
- Initial tension during curing and excavation to subgrade 12/11/04 – 12/18/04
- Mat placement 12/24
- Theatre construction 1/05 – 3/05
- Fill placement 3/14/05 – 3/20/05



- Forming and concrete placement load/unload at interior location on mat

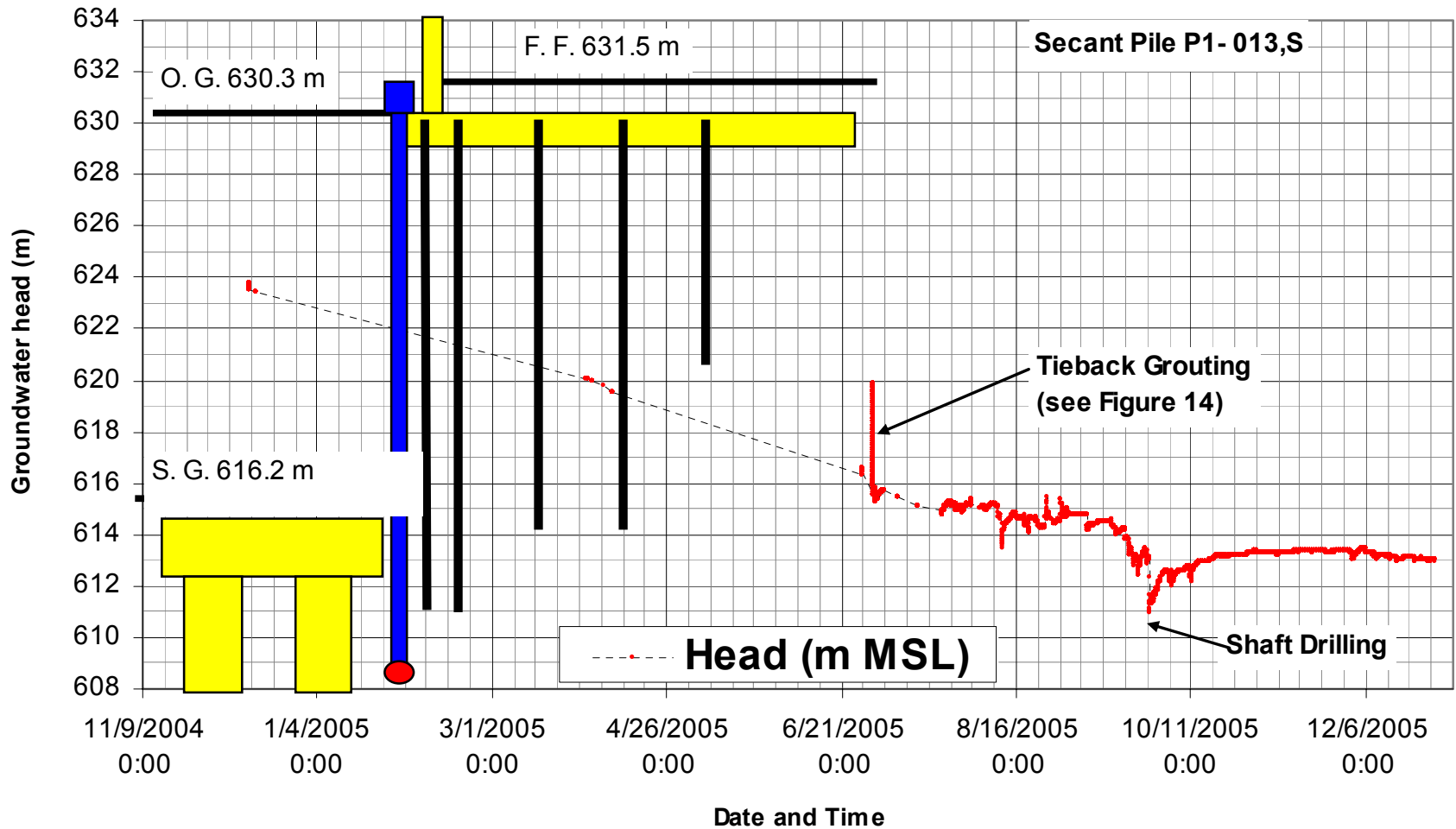


- Tieback stressing effects
- 15 Tiebacks at Level -1 stressed

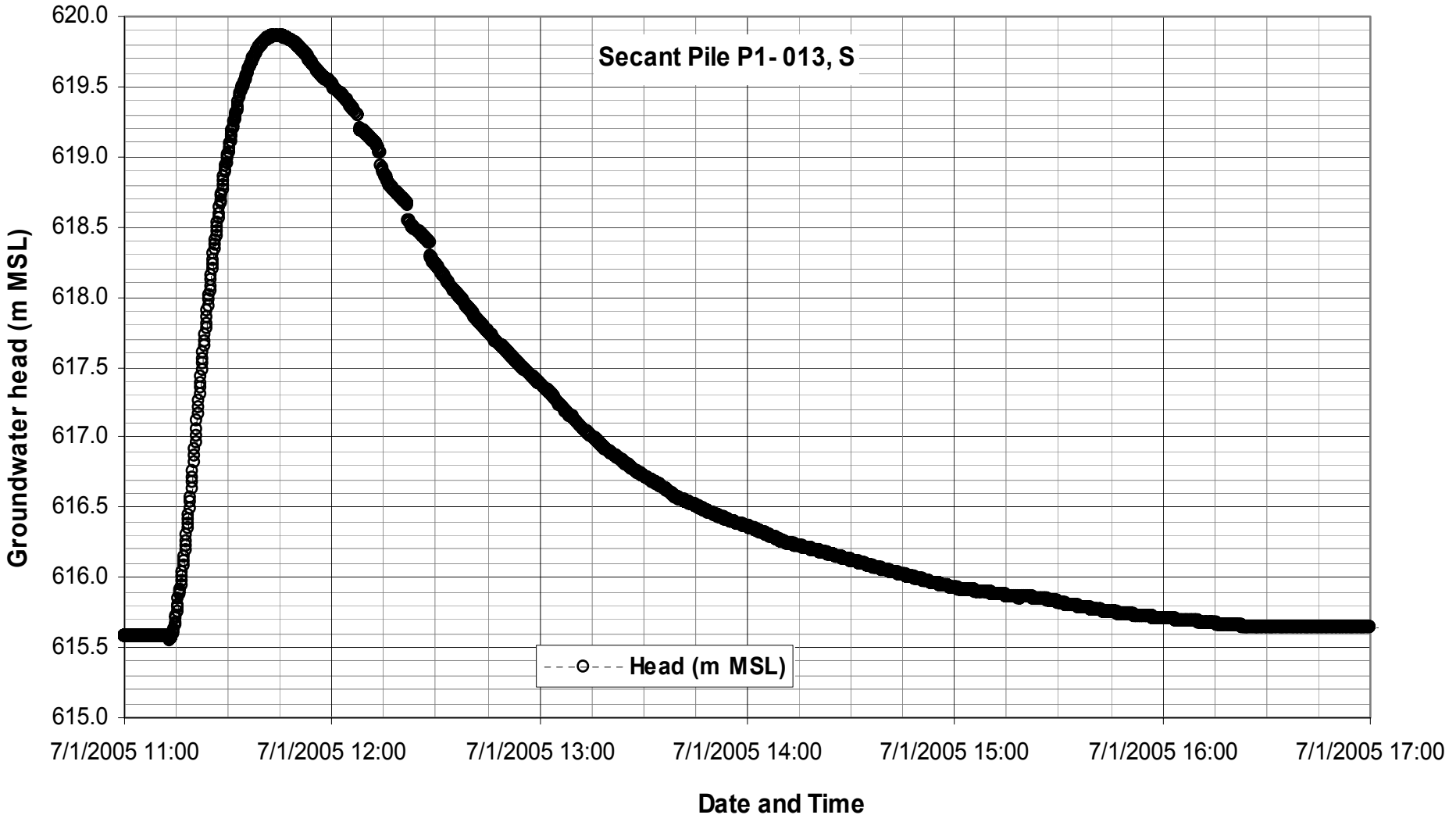


- Inclinometer data record
- Weekly record 4/05 to 8/05 and 2/06

- Hourly data by IPI system 8/05 – 12/05 not included

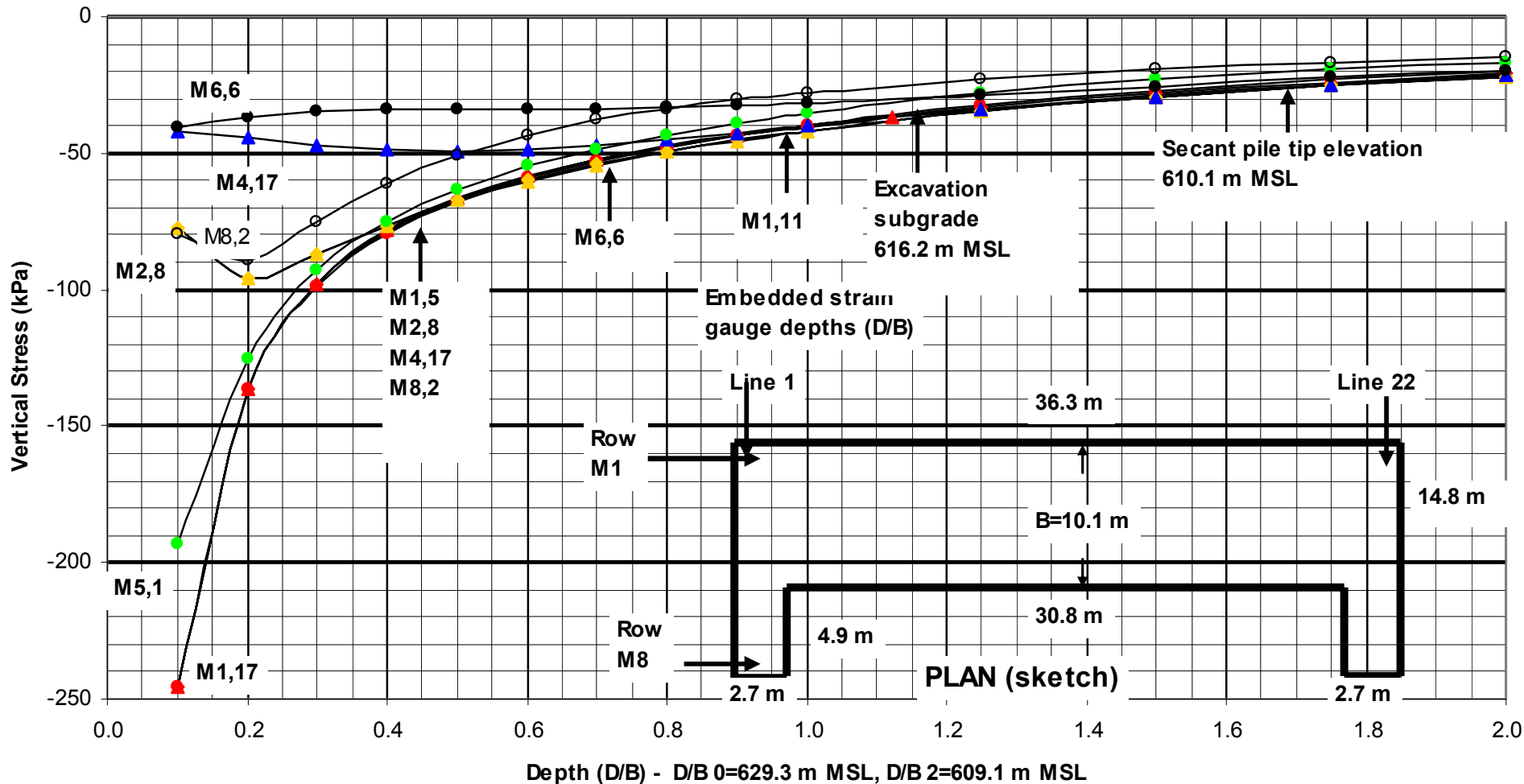


- Piezometer data record 12/04 – 1/06
- Head rise during tieback grouting
- Head drop during drilled shaft construction



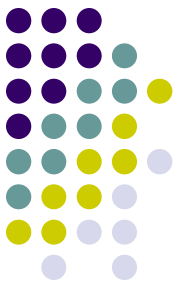
- Tieback grout placement at Level – 2

Elastic Analyses vs. Observations



- Boussinesq elastic analyses by superposition
- Instrumented micropile locations and depths

Ground/Micropile Load Sharing Pre-Excavation, April 1, 2004



| Location | D/L | D/B | 4/1/05 Load (kN) | Boussinesq Stress (kPa) | Tributary Area (m ²) | Stress Ratio % |
|----------|------|-----|------------------|-------------------------|----------------------------------|----------------|
| M1,5 | 0.30 | 0.5 | -41.08 | -67.5 | 1.62 | 37.6 % |
| M1,11 | 0.66 | 1.1 | -52.41 | -36.7 | 1.62 | 88.3 % |
| M1,17 | 0.30 | 0.5 | -55.05 | -58.7 | 1.62 | 50.9 % |
| M5,1 | 0.57 | 0.8 | -42.62 | -43.2 | 1.96 | 50.4 % |
| | | | | | | |
| N2,2 | 0.66 | 1.1 | -50.32 | -34.0 | 2.02 | 73.2 % |
| M2,8 | 0.30 | 0.5 | -14.02 | -67.4 | 3.70 | 5.6 % |
| M2,14 | 0.30 | 0.5 | -69.93 | -67.3 | 3.70 | 28.1 % |
| M2,20 | 0.30 | 0.5 | -50.00 | -72.0 | 4.18 | 16.6 % |
| M8,2 | 0.47 | 0.5 | -64.71 | -50.9 | 2.70 | 47.0 % |
| | | | | | | |
| M4,10 | 0.60 | 0.8 | -26.55 | -43.3 | 5.64 | 10.9 % |
| M4,17 | 0.37 | 0.5 | -32.94 | -49.4 | 5.64 | 11.8 % |
| | | | | | | |
| M6,6 | 0.58 | 0.8 | -30.26 | -33.4 | 5.62 | 17.1 % |

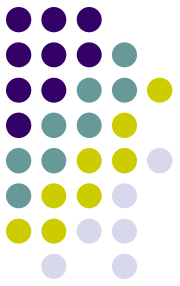
- 37.6% to 88.3% at perimeter
- 5.6% to 73.2% at 1st interior row
- 10.9% to 11.8% near middle of mat (row 4)
- 17.1% at back edge of mat (row 6)
- Prior to stressing

Ground/Micropile Load Sharing Post Construction January 31, 2006



| Location | D/L | D/B | 1/31/06 Load (kN) | Boussinesq Stress (kPa) | Tributary Area (m ²) | Stress Ratio % |
|----------|------|-----|-------------------|-------------------------|----------------------------------|----------------|
| M1,5 | 0.30 | 0.5 | -22.77 | -67.5 | 1.62 | 20.8 % |
| M1,11 | 0.66 | 1.1 | -68.56 | -36.7 | 1.62 | 115.5 % |
| M1,17 | 0.30 | 0.5 | -25.22 | -58.7 | 1.62 | 26.6 % |
| M5,1 | 0.57 | 0.8 | -56.18 | -43.2 | 1.96 | 66.4 % |
| | | | | | | |
| N2,2 | 0.66 | 1.1 | -59.43 | -34.0 | 2.02 | 86.1 |
| M2,8 | 0.30 | 0.5 | -16.60 | -67.4 | 3.70 | 6.7 % |
| M2,14 | 0.30 | 0.5 | -198.27 | -67.3 | 3.70 | 79.6 % |
| M2,20 | 0.30 | 0.5 | -87.14 | -72.0 | 4.18 | 29.0 % |
| M8,2 | 0.47 | 0.5 | 252.84 | -50.9 | 2.70 | 184 % * |
| | | | | | | |
| M4,10 | 0.60 | 0.8 | 201.22 | -43.3 | 5.64 | 83.0 %* |
| M4,17 | 0.37 | 0.5 | -31.71 | -49.4 | 5.64 | 11.4 % |
| | | | | | | |
| M6,6 | 0.58 | 0.8 | 261.76 | -33.4 | 5.62 | 139.5 %* |

- After tieback stressing
- 20.8% to 115.5% at perimeter
- 6.7% to 184% (tension) at 1st interior row
- 11.4% to 83.0% (tension) near middle of mat (row 4)
- 139.5% (tension) at back of mat (row 6)



CONCLUSIONS

- ❑ The micropiles accumulated 10 to 90 percent of the load as it was applied in proportion to the relative stiffness between the soils and the micropiles.
- ❑ Instrumented micropiles responded with strains consistent with their location within the group and the forces applied.
- ❑ The micropiles provided confinement and resistance to axial deformation during tieback stressing.
- ❑ Tie back stressing caused micropiles to act in tension at the tieback bond zone.